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JC892 U.S. PTO

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A Named Inventor/Application Identifier: Donald W. Allen, Dean L. Henning, David W. McMillan, Richard B. McDaniel and Kenneth Dupal
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Title: SMOOTH SLEEVES FOR DRAG AND VIV REDUCTION OF CYLINDRICAL STRUCTURES
Date: July 26, 2000

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07/26/00

UTILITY PATENT APPLICATION TRANSMITTAL
UNDER 37 CFR 1.53(b)

Assistant Commissioner for Patents
Box Patent Applications
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1. ☒ This application is a(n):
- a. ☒ Original
- b. ☐ Continuation-in-part of Application Serial No. _____ filed _____
- c. ☐ Divisional of Application Serial No. _____ filed _____
☐ Applicant(s) elect the invention of Group/Species _____
- d. ☐ Continuation of Application Serial No. _____ filed _____
2. ☒ Specification
- a. ☒ Pages 12
- b. ☒ Drawings, Total sheets 8
3. ☒ Oath or Declaration
- a. ☒ Newly executed (original or copy)
- b. ☐ Copy from a prior application
☐ Please delete the following named inventors in the prior application: _____
4. ☒ Please amend the specification
- a. ☐ By inserting before the first line:
This is a ☐ continuation ☐ division ☐ continuation-in-part of Application Serial No. _____ filed _____, the entire disclosure of which is hereby incorporated by reference
- b. ☒ By inserting before the first line:
This application claims the benefit of U.S. Provisional Application No. 60/154,289 filed September 16, 1999, the entire disclosure of which is hereby incorporated by reference
- c. ☐ Cancel claims _____
5. ☐ This application claims the benefit of Application Number _____ filed on _____ in _____ under 35 U.S.C. § 119, § 365(a), or § 365(b).
(For originals)

6. ☐ Microfiche Computer Program (Appendix)
7. ☐ Recognize as an associate attorney _____, Registration No. _____
8. ☒ Address all future communications to:

Mark A. Smith
 Shell Oil Company
 Legal – Intellectual Property
 P. O. Box 2463
 Houston, Texas 77252-2463

9. ☒ Fee Transmittal (duplicate enclosed)

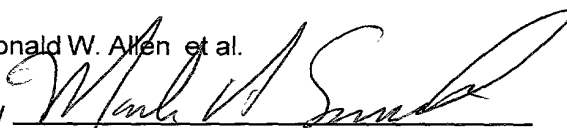
(1) FOR	(2) NUMBER FILED	(3) NUMBER EXTRA	(4) RATE	(5) CALCULATIONS
TOTAL CLAIMS (37 CFR 1.16(c))	6- 20 =		X \$18.00 =	\$0.00
INDEPENDENT CLAIMS (37 CFR 1.16(b))	3- 3 =		X \$78.00 =	0.00
MULTIPLE DEPENDENT CLAIMS (if applicable) (37 CFR 1.16(d))			+ \$260.00 =	0.00
			BASIC FEE (37 CFR 1.16(a))	\$690.00
Total of above Calculations =				0.00
TOTAL =				\$690.00

10. ☒ Please charge Deposit Account No. 19-1800 in the amount of \$690.00.
11. ☒ The Assistant Commissioner is authorized to charge all additional required fees or to credit overpayments, to Deposit Account No. 19-1800, including fees required under 37 CFR 1.17
12. ☒ Accompanying Application Parts
- a. ☐ Recordal of Assignment and Assignment
- b. ☐ Information Disclosure Statement/PTO-1449
- c. ☐ Preliminary Amendment
- d. ☒ A self-addressed, stamped return receipt postcard to be returned with the filing date and Serial No. thereon
- e. ☐ Certified copy of priority documents

Respectfully submitted,

Donald W. Allen et al.

By



Their Attorney, Mark A. Smith
 Registration No. 30,220
 (713) 241-2094

P. O. Box 2463
 Houston, Texas 77252-2463

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SMOOTH SLEEVES FOR DRAG AND VIV REDUCTION OF CYLINDRICAL STRUCTURES

BACKGROUND

10 The present invention relates to a method and apparatus for reducing
drag and vortex- induced-vibrations ("VIV") and, more particularly, reducing VIV and
drag to cylindrical elements in marine environments.

Production of oil and gas from offshore fields has created many unique
engineering challenges. One set of such challenges involves the use of cylindrical
marine elements that are susceptible to large drag and vibrations when in the
presence of significant ocean currents. Such marine elements are used in a variety of
5 applications, including, e.g., subsea pipelines; drilling, production, import and export
risers; tendons for tension leg platforms; legs for traditional fixed and for compliant
platforms; space-frame members for platforms; cables; umbilicals; and other mooring
elements for deepwater platforms; and, although not conventionally thought of as
20 such, the hull and/or column structure for tension leg platforms (TLPs) or for spar type
structures. These currents cause drag on the element and cause vortexes to shed
from the sides, inducing drag forces and vibrations that can lead to the failure of the
marine elements. Large drag forces can result in increased mooring or station
keeping costs as well as the imposition of constraints on what kinds of systems are
25 workable in a current environment (due to stress limitations, top angle limitation
while drilling, etc.). Large vibrations (primarily vortex-induced vibrations) cause
dynamic motions that, in turn, cause premature fatigue failures of structural

members. In addition, large vibrations typically cause substantial increases in mean and dynamic drag forces. Finally, the presence of ocean currents can cause interference between adjacent structures.

One solution to the above set of issues is to use helical strakes.

5 However, helical strakes are not very effective at reducing drag, and those are rarely used if drag reduction is important (e.g. drilling risers). Another solution which, if properly designed, can have all the positive benefits of helical strakes and can also reduce drag, is the use of fairings. However, there are many instances where the use of fairings is either impractical or uneconomical. An example is the reduction of drag and VIV for a drilling riser, where fairings can be very difficult to handle and therefore impose large usage costs in terms of lost time due to installation. For instance, fairings will not fit through a drilling rig rotary in order to allow installation above the rotary at a substantially reduced cost. Fairings also must typically be quite large and expensive to minimize drag coefficients. One of these challenges is dealing with effects of currents on fixed cylindrical marine elements.

SUMMARY OF THE INVENTION

The present invention is a method of controlling drag and vortex induced vibration in a substantially cylindrical element by providing an ultra-smooth surface about the cylindrical element. Another aspect of the present invention is a system for controlling drag and vortex induced vibration in which a substantially cylindrical marine element has an ultra-smooth effective surface.

BRIEF DESCRIPTION OF THE DRAWINGS

The brief description above, as well as further objects and advantages of the present invention, will be more fully appreciated by reference to the following

detailed description of the preferred embodiments which should be read in conjunction with the accompanying drawings in which:

FIG. 1 is a top elevational view of one embodiment of the invention formed sleeve;

FIG. 2 is a side elevational view of the sleeve of FIG. 1, taken at line 2-2 in FIG. 1;

FIG. 3 is side elevational view of a hinge of FIG. 1;

FIG. 4 is a side elevational view of a latch of FIG. 1;

FIG. 5 is a side elevational view of a secured latch;

FIG. 6 is a top elevational view of an installed sleeve;

FIG. 7 is a side elevational view of a drilling riser;

FIG. 8 is a side elevational view of a sleeve installed on a drilling riser;

FIG. 9 is a cross sectional top view of a sleeve being installed about a riser;

FIG. 10 is a cross sectional top view of the sleeve of FIG. 9 now installed about a drilling riser;

FIG. 11 is a cross sectional side view taken at line 11-11 in Fig. 9 (from which the riser, centralizers and control lines have been removed for simplification);

FIG. 12 is a side elevational view of a drilling riser section;

FIG. 13 is a side elevational view of an alternate embodiment of a sleeve installed about the riser;

FIG. 14 is a side elevational "movie" view of sleeve handling procedures;

FIG. 15 is a graph of VIV as a function of Reynolds Number; and

FIG. 16 is a graph of drag coefficient as a function of Reynolds Number.

A DETAILED DESCRIPTION OF ILLUSTRATIVE EMBODIMENTS

FIGS. 1 and 2 illustrate a substantially cylindrical sleeve 10 presenting an ultra-smooth surface 12. Here the sleeve is a clam-shell design formed of fiberglass with a gel-coat presenting ultra-smooth surface 12. Opposing sides of the clam-shell are secured with hinges 14 and connectors such as latches 16 which may be secured with a hairpin 18 in one embodiment of the present invention. See also FIG. 3-4. Lifting provisions may be conveniently provided with lifting eyes 22. Ribs 20 provide some strength to the sleeve 10 and may be formed to axially secure the sleeve about riser sections.

FIG. 6 illustrates sleeve 10 secured about axially cross sectioned drilling riser 24. A dotted outline also illustrates the diameter of the rotary on the offshore platform. Even though the sleeve is configured to encircle a drilling riser 24, its buoyancy modules 26, and attendant control lines 28, it remains sufficiently narrow to pass through the rotary so that installation and removal can be accomplished above the rotary.

In this embodiment, it is desired for sleeves 10 to have a substantially shorter length than that of buoyancy module 26 and an additional groove 32 is formed in the outer circumference of the buoyancy module. See FIG. 7. Ribs 20 on the inside of the sleeve sections engage the top 30 of the buoyancy module or the groove, respectively. See sleeve sections 10A and 10B in FIG. 8.

FIGS. 10-11 illustrate another embodiment. Here drilling riser 24 is afforded buoyancy modules 26 at intervals and the control lines 28 are surrounded intermittently with riser centralizers 34. Note how ribs 20 are provided seats 36 to form

around the control lines/buoyancy modules and to rest on centralizers 34. FIGS. 9 and 10 illustrate sleeve installation with the clam-shell capture of the drilling riser. Note also that the standoff of mux line 38 folds to a position within sleeve 10.

FIGS 12-13 illustrate another embodiment, here for using half length sleeve sections 10 with full length buoyancy modules 26. In this instance two types of sleeve sections are used, hanging sleeve 10A and stacking sleeve 10B. The hanging sleeve engages to the top surface of the buoyancy module and any centralizer presented there. Whereas the stacking sleeve 10B can be configured to engage to the bottom of hanging sleeve 10A or to rest on top of the next lower hanging sleeve 10C and the ribs are configured accordingly. See FIG. 13.

FIG. 14 illustrates one option for sleeve handling. It is a "movie" of running sleeves 10 on cables 42 operated by a crane (not shown). The assembly/disassembly operation (see FIGS. 9 and 10) is conducted above rotary opening 40. This greatly simplifies handling and storage of the sleeve sections.

Another possibility facilitated by overall dimensions that can pass through the rotary is installing the sleeve sections on an installed drilling riser. In this embodiment the sleeve is near neutrally buoyant, made up above the rotary, lowered to the ocean surface and released. The ribs, if any, are configured to allow easy sliding of the sleeve and an array of sleeves is stacked, one on another, as concentrically symmetrical sleeves slide along the drilling riser.

Alternatively, the sleeve sections may be installed below the rotary, whether installed at the time of riser deployment or installed later.

The illustrated examples use gel-coated fiberglass. However, the ultra-smooth surface could be provided by sleeves made of copper (when marine growth

inhibition is required), carbon fiber, rubber, or any sufficiently smooth thermoplastic, metal alloy, or other material. The smooth surface may even be obtained by the surface finish on the outside of the cylindrical element or maintained by a ablative paint or other coating applied to the surface of the element.

5 If sleeves are used to present the substantially cylindrical ultra-smooth surface, there are a number of alternatives to construct and attached or install the sleeves. For instance, the sleeve can be clam-shelled around the cylindrical element using hinges and alternative latching mechanisms such as snaps, bolts, or other fasteners. Alternatively, the sleeves can be made with a continuous circumference and slid over a cylindrical element. Or there are other alternatives for constructing a sleeve form one or more sections. For instance, the sleeve need not be constucted of halves, each covering an approximately equal amount of the circumference. A C sleeve (a sleeve that covers more than 180 degrees of the circumference but less than 360 degrees of the circumference) can be made with the rest of the circumference optionally enclosed by a second piece that completes the circumference. The C shaped sleeve can be clam-shelled around the cylindrical element using hinges and a latching mechanism, or can be slid over the structure. Further, sleeves, or sleeve sections, covering all or part of the circumference, can be held in place using hardware that is attached to the cylindrical element itself. This hardware can include latches, receptacles for bolts, pins, rivets, screws, or other fasteners. Or, a sleeve that consists of two or more parts, which make up the circumference, can be made such that the parts are held together by straps or banding materials. This includes the possibility of providing grooves in the cylindrical element to allow for strapping materials. Further, the sleeves can be pre-

installed , they can be installed on the cylindrical element during its installation (e.g. while running a drilling riser); or they can be installed after the cylindrical element has already been installed (a post-installation).

While there are many ways to provide it, a critical aspect is the ultra-smooth surface. The drag coefficient for flow past a cylinder sharply decreases as the Reynolds number is increased beyond about 200,000 (called the "critical" Reynolds number range) and then slowly recovers (called the "supercritical" Reynolds number range). While it was recognized that and surface roughness can effect the Reynolds number at which this "dip" occurs and can add to the drag coefficient, conventional wisdom held that cylindrical elements should experienced substantial VIV accompanied by fairly large drag at critical and supercritical Reynolds number ranges.

But, surprisingly, it was discovered that a very smooth cylinder would not experience VIV in this Reynolds number range, and furthermore this cylinder would experience very low drag. Further, the an "ultra-smooth" sleeve can be effective in Reynolds number ranges from about 200,000 to over 1,500,000, perhaps more. In fact, benefits begin to be seen in the VIV and drag at a Reynolds number of about 100,000.

This relationship of VIV and drag as a function of the level of surface roughness has been found to be quantifiable in a dimensionless roughness parameter, K/D , where:

K is the average peak to trough distance of the surface roughness (e.g., as measured using confocal scanning with an electron microscope); and

D is the effective outside diameter of the cylindrical element, including any sleeve or coating.

Substantial reduction in VIV can be observed where K/D is less than about 1.0×10^{-4} and most pronounced at about 1.0×10^{-5} or less for fairly uniform roughness densities. A higher K/D ratio may allow achieving the same results where the roughness density decreases.

FIGS. 15-16 illustrate test results demonstrating the surprising practicality and effectiveness of ultra-smooth surfaces. These tests were conducted in a tow tank environment with the marine element towed to develop relative motion between the test subject and the water. FIG. 15 illustrates transverse RMS displacement as a function of Reynolds number for an ultra-smooth cylinder and for relatively rough cylinders representing marine elements. FIG. 16 illustrates drag coefficient as a function of Reynolds number for the same samples. The dimensionless roughness parameter K/D for these samples were:

ultra-smooth 5.1×10^{-5}

Rough #1 1.9×10^{-4}

Rough #2 2.5×10^{-3}

Rough #3 5.8×10^{-3}

Improvement to both suppression of VIV excitement and drag was observed and very pronounced at $K/D = 5.1 \times 10^{-5}$.

It should be appreciated that this improvement in the ability to control both drag and VIV beneficially impacts offshore operations. For instance, in drilling riser applications, this could reduce or eliminate down time due to ocean currents, including loop current phenomena. On production risers, enhanced drag and VIV

reduction can allow closer spacing of risers without interference problems. Further, this could impact the design of TLPs or spars in high current areas by eliminating, or reducing, the need for more expensive methods and devices.

Although the illustrative examples are principally drilling risers, those having ordinary skill in the art and the benefit of this disclosure could apply this invention to any number of cylindrical members including, but not limited to, subsea pipelines; production, import and export risers (catenary or not); tendons for tension leg platforms; legs for traditional fixed and for compliant platforms; space-frame members for platforms; cables; umbilicals; other mooring elements for deepwater platforms; and hull and/or column structures for tension leg platforms (TLPs) or for spar type structures.

Other modifications, changes, and substitutions are also intended in the forgoing disclosure. Further, in some instances, some features of the present invention will be employed without a corresponding use of other features described in these illustrative embodiments. Accordingly, it is appropriate that the appended claims be construed broadly and in a manner consistent with the spirit and scope of the invention herein.

WHAT WE CLAIM IS:

1. A method of controlling drag and vortex induced vibration in a substantially cylindrical element comprising providing an ultra-smooth surface about the cylindrical element.

5 2. A method of controlling drag and vortex induced vibration in accordance with Claim 1 wherein providing the ultra-smooth surface comprises providing a coating having a K/D ratio of about 1.0×10^{-4} or less where:

K is the average peak to trough distance; and

D is the effective outside diameter of the cylindrical element, including the coating.

3. A method of controlling drag and vortex induced vibration in accordance with Claim 1 wherein providing the ultra-smooth surface comprises providing a substantially cylindrical sleeve having a K/D ratio of about 1.0×10^{-4} or less where:

K is the average peak to trough distance; and

D is the effective outside diameter of the cylindrical element, including the sleeve.

4. A system for controlling drag and vortex induced vibration, comprising:

a substantially cylindrical marine element; and

20 an ultra-smooth effective surface about the substantially cylindrical marine element.

5. A system in accordance with Claim 4 wherein the ultra-smooth cylindrical surface is a coating material having a K/D roughness parameter of about 1.0×10^{-4} or less where:

K is the average peak to trough distance; and

D is the effective outside diameter of the cylindrical element, including the coating.

6. A system in accordance with Claim 4 wherein the ultra-smooth cylindrical surface is a substantially cylindrical sleeve substantially surrounding the marine element having an outside K/D roughness parameter of about 1.0×10^{-4} or less where:

K is the average peak to trough distance; and

D is the effective outside diameter of the cylindrical element, including the sleeve.

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SMOOTH SLEEVES FOR DRAG AND VIV REDUCTION
OF CYLINDRICAL STRUCTURES

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ABSTRACT OF THE DISCLOSURE

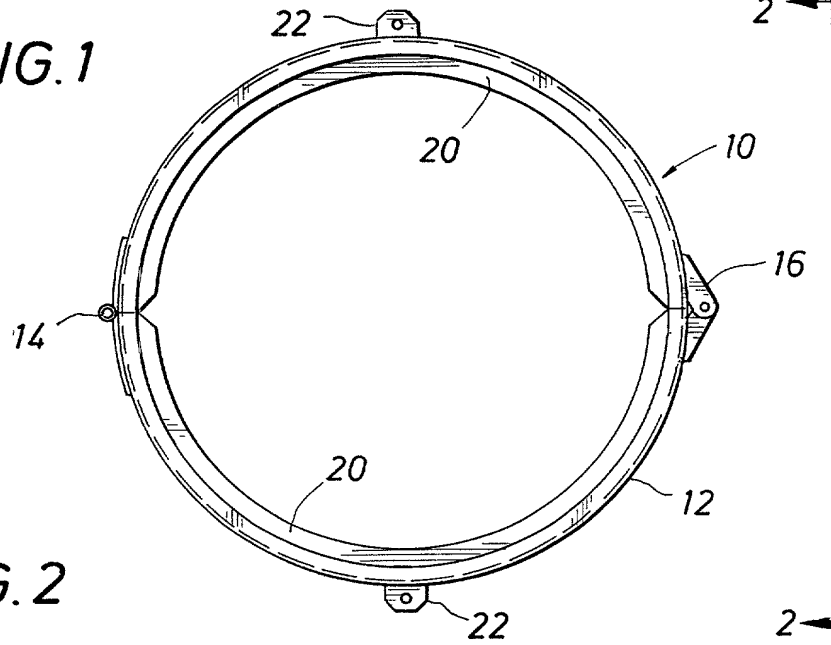
A method is disclosed for controlling drag and vortex induced vibration in a substantially cylindrical element by providing an ultra-smooth surface about the cylindrical element. A system is also disclosed for controlling drag and vortex induced vibration in which a substantially cylindrical marine element has an ultra-smooth effective surface.

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FIG. 1



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FIG. 2

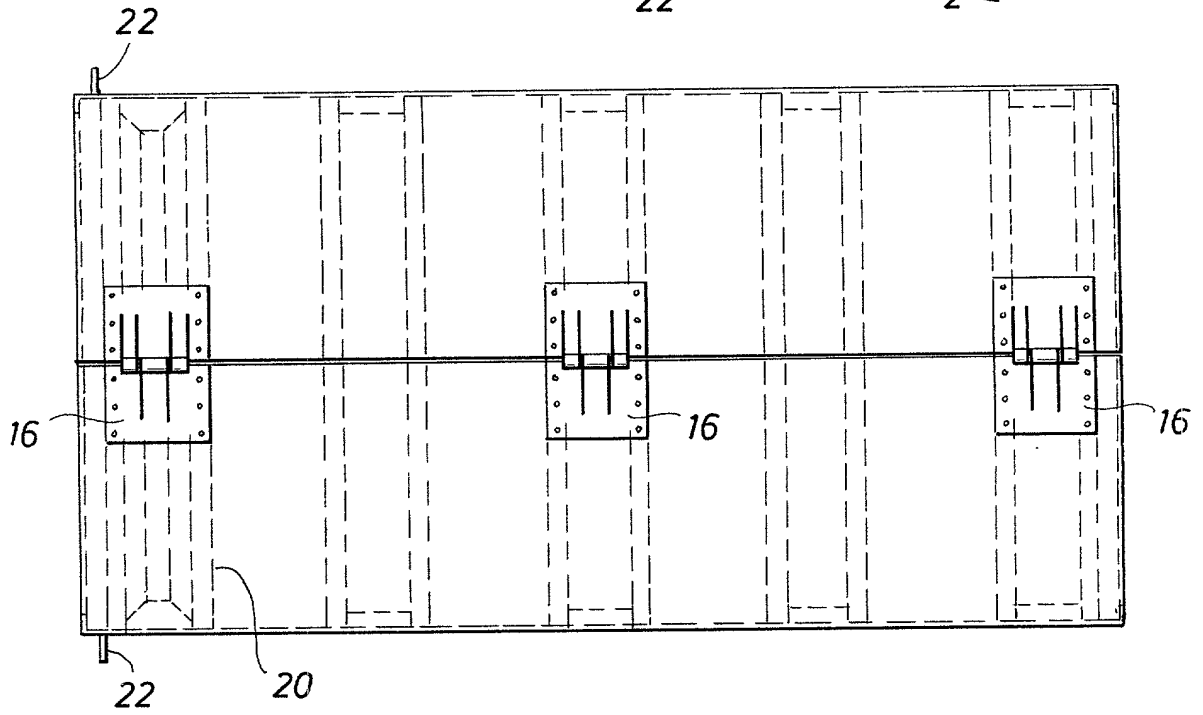


FIG. 3

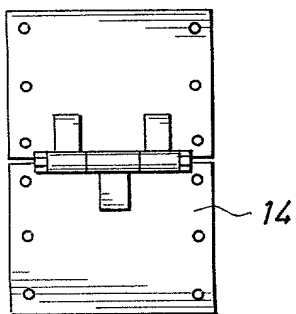


FIG. 4

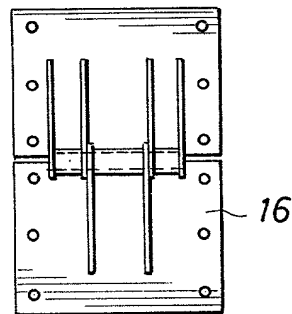
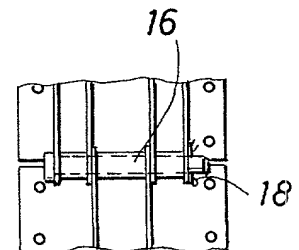


FIG. 5



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FIG. 6

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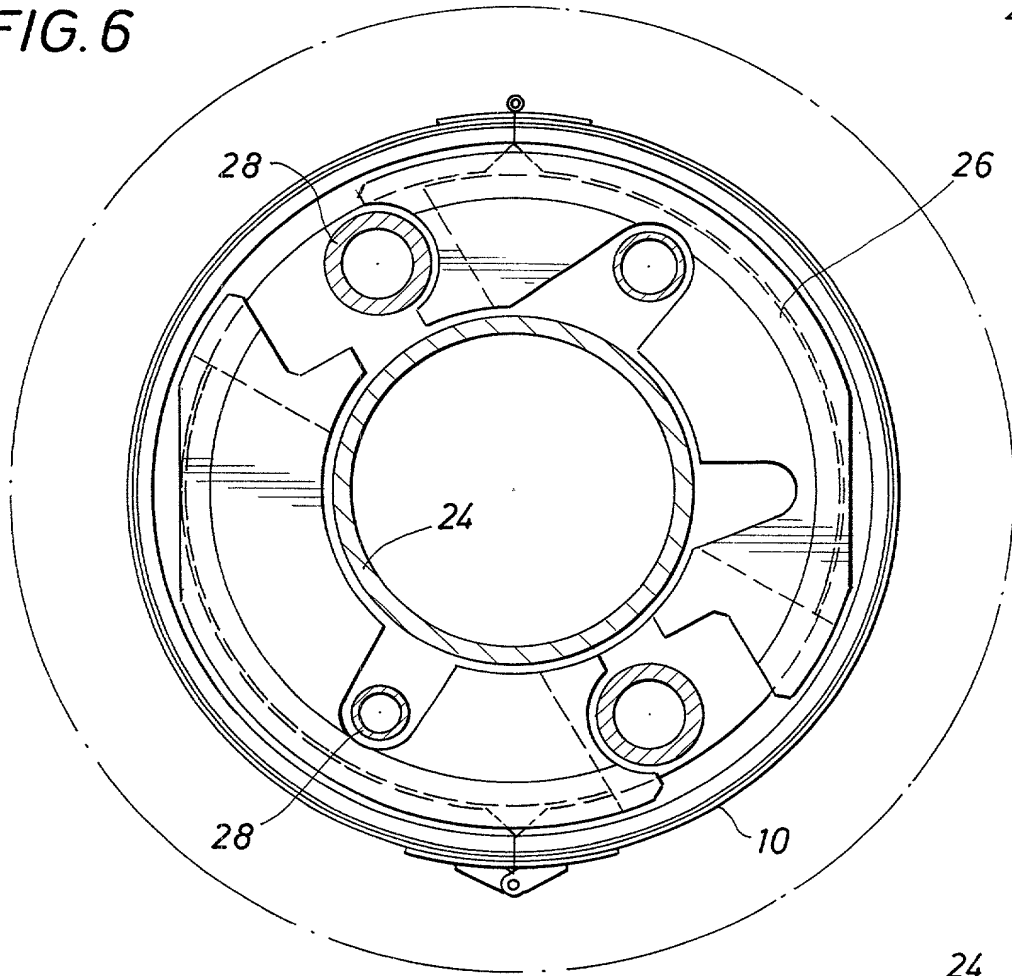


FIG. 7

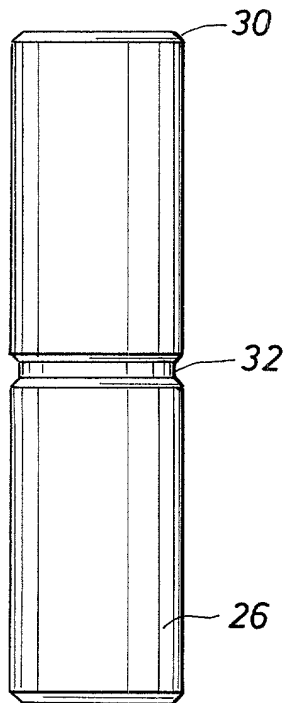
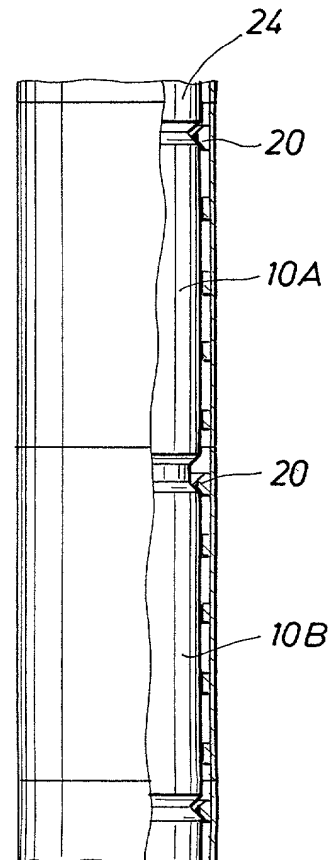


FIG. 8



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FIG.10

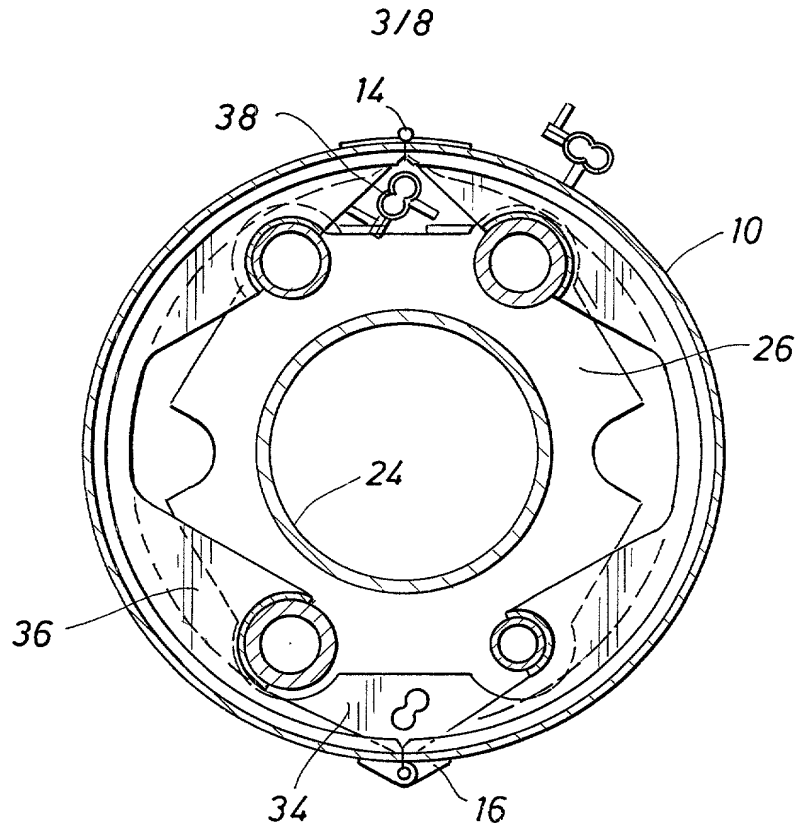
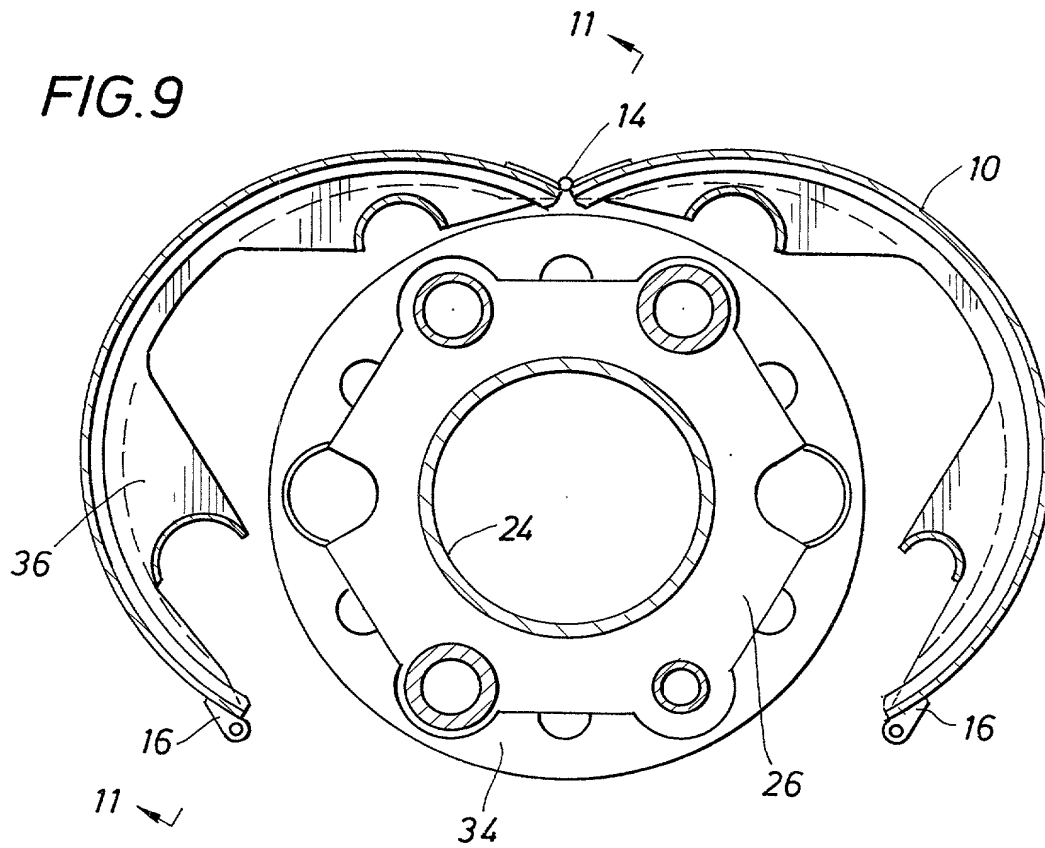


FIG.9



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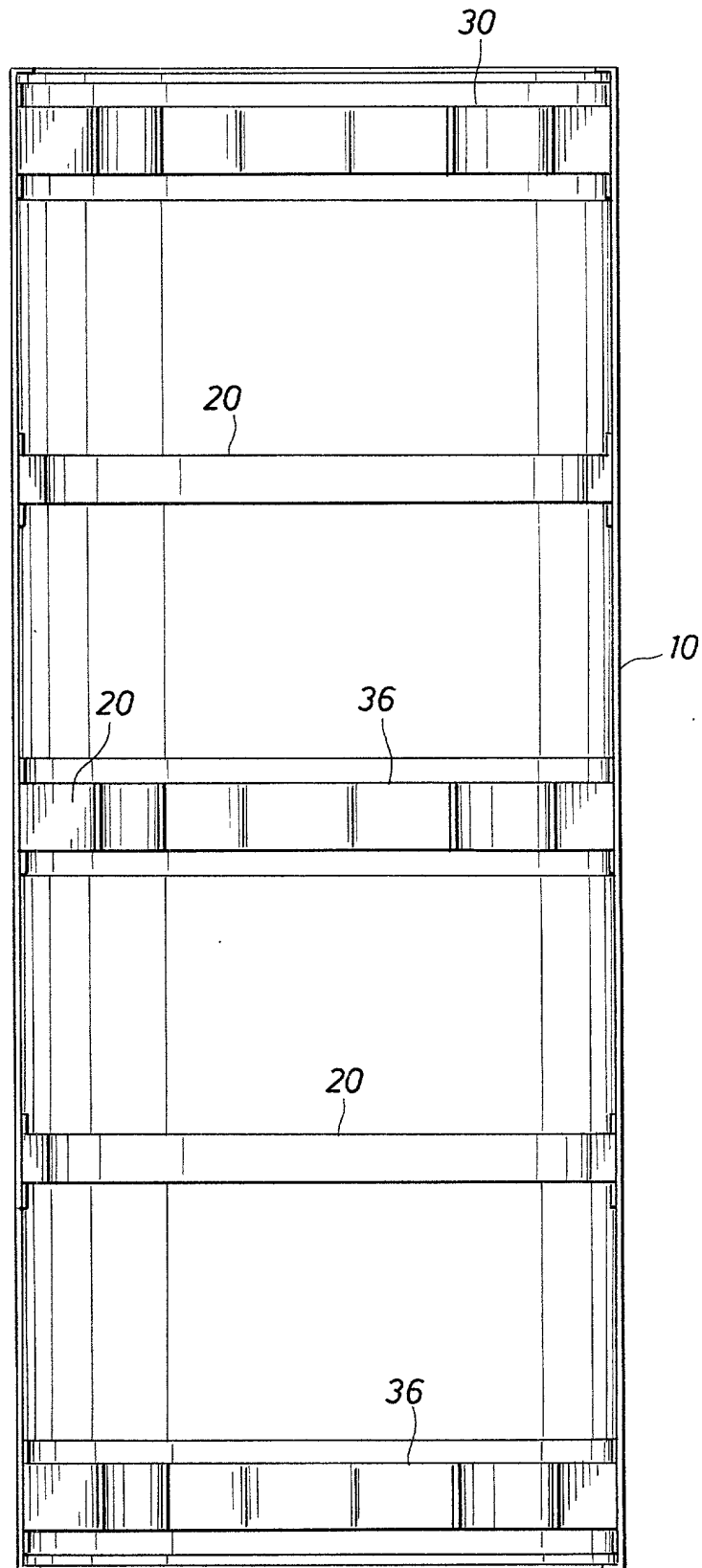


FIG.11

FIG. 12

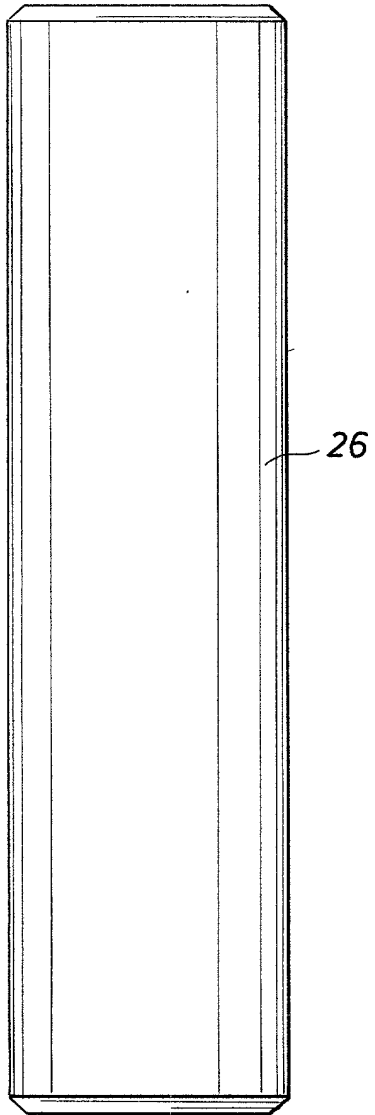


FIG. 13

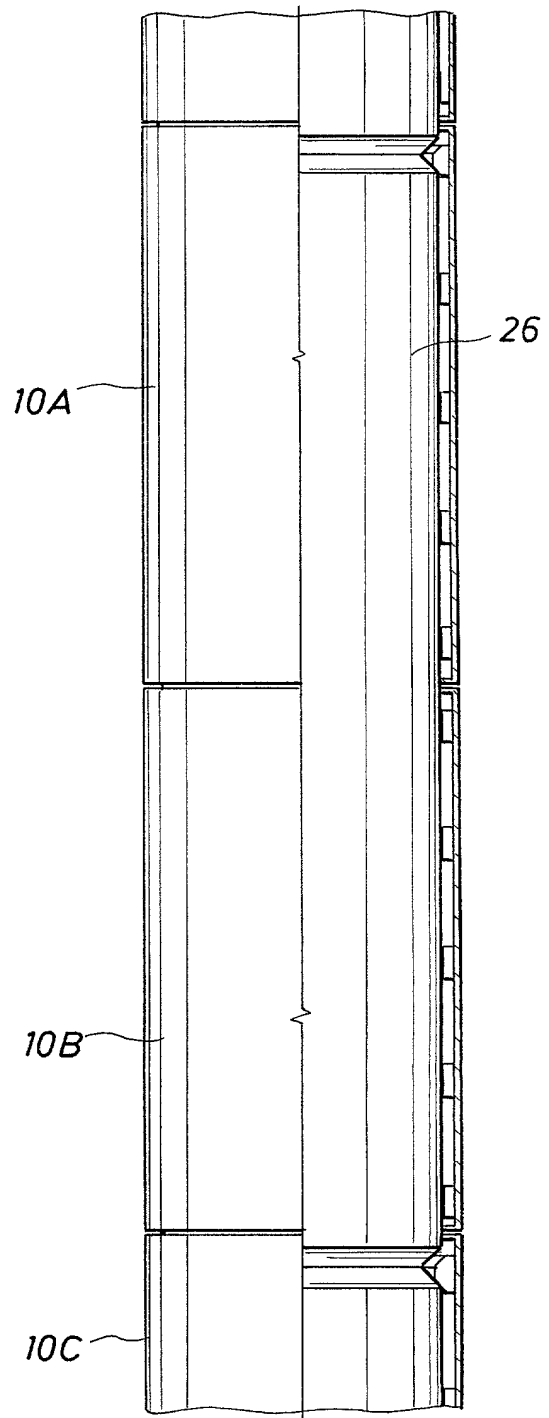


FIG. 14

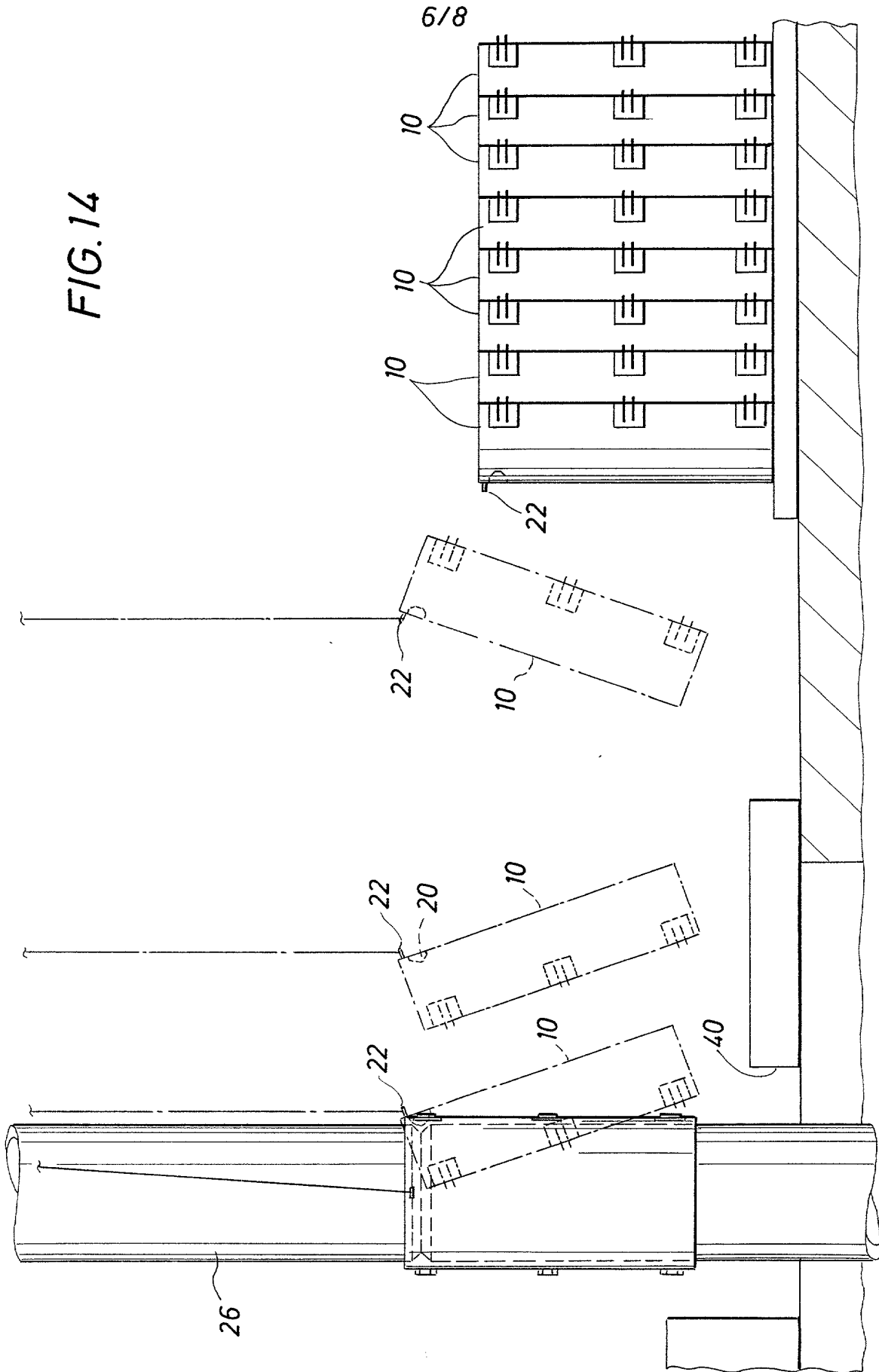


FIG.15

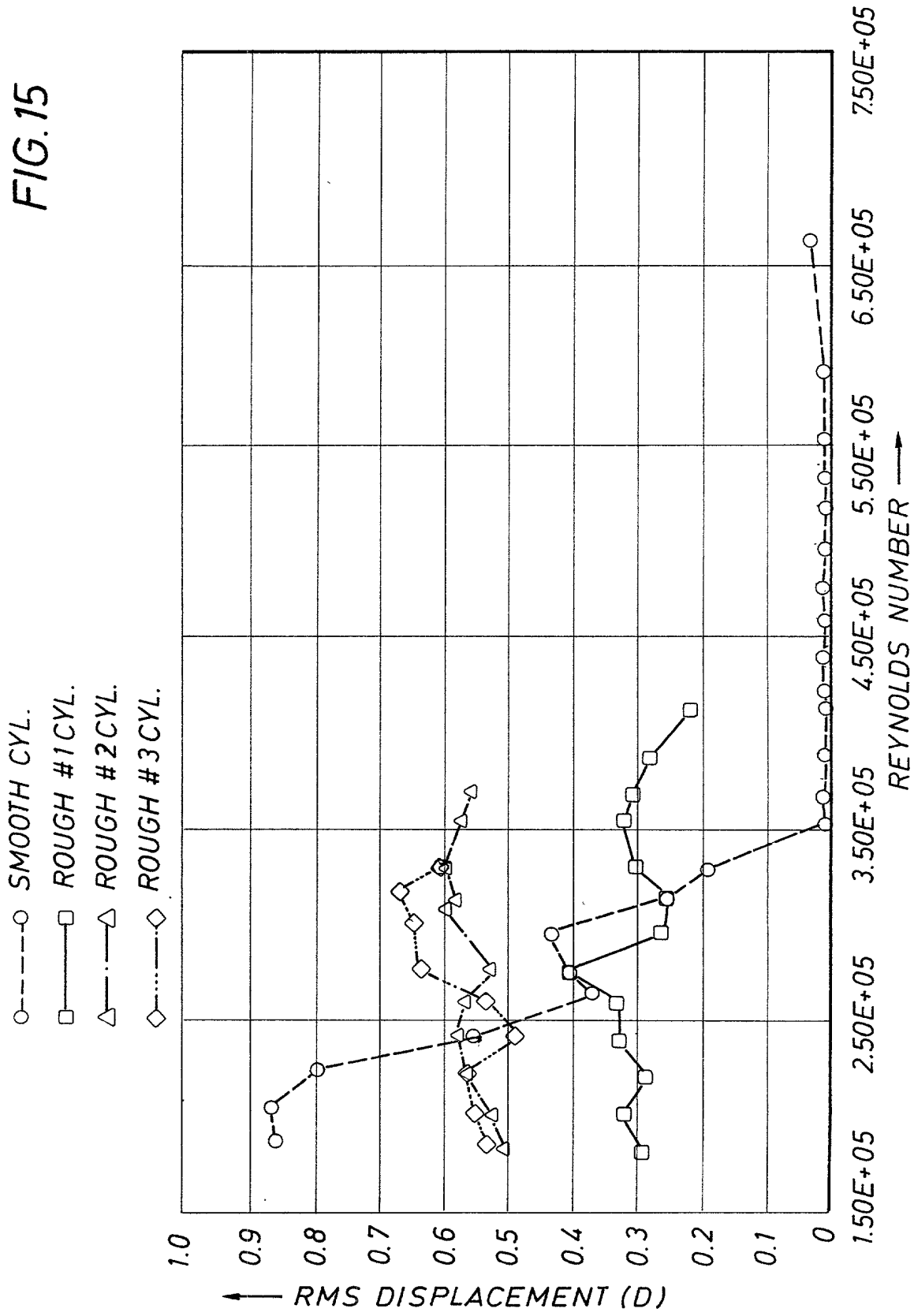
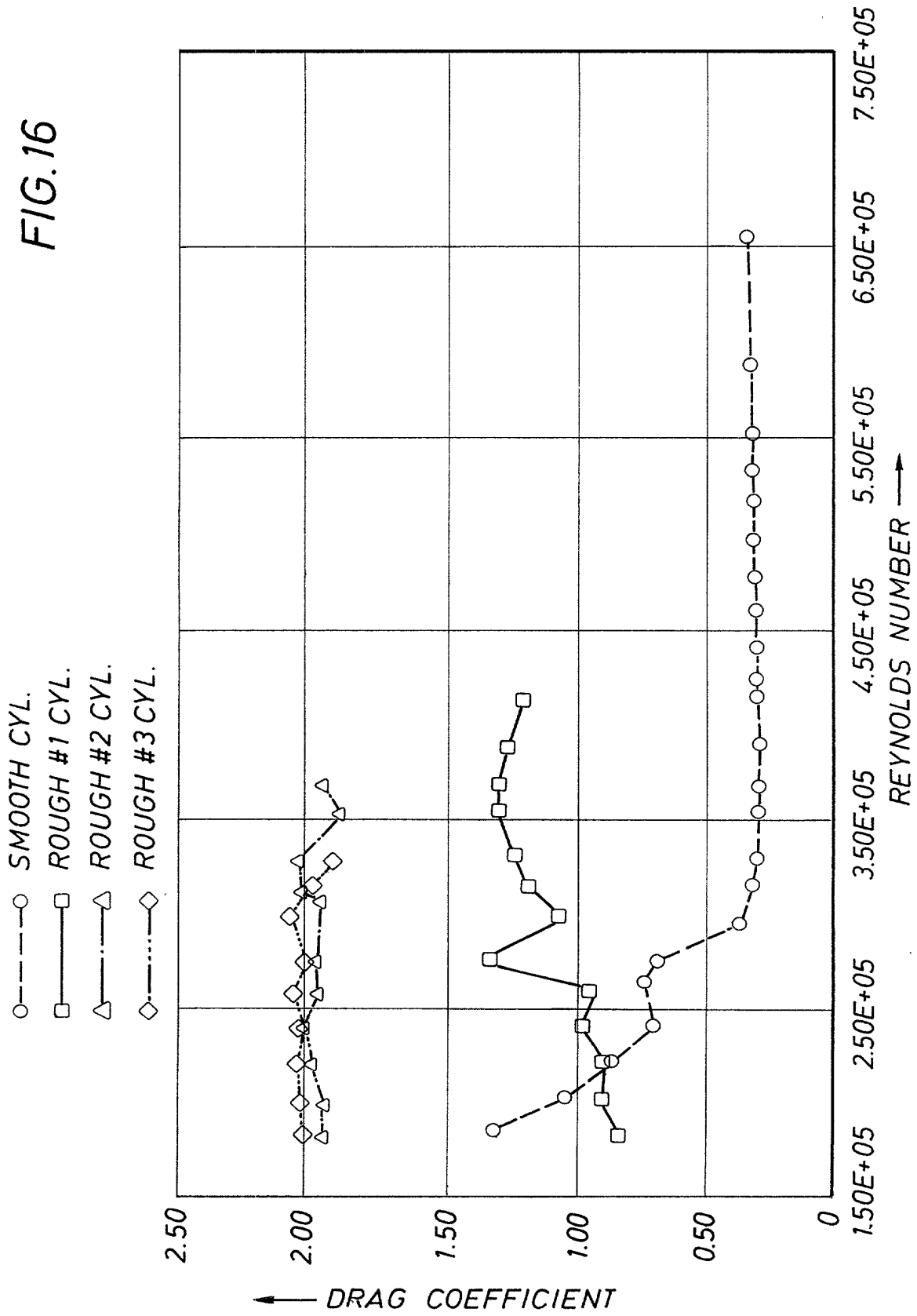


FIG. 16



DECLARATION AND POWER OF ATTORNEY FOR PATENT APPLICATION

ATTORNEY'S DOCKET NO.
TH-1258 (US)
MAS:KNL

As a below named inventor, I hereby declare that:

My residence, post office address, and citizenship are as stated below next to my name. I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled SMOOTH SLEEVES FOR DRAG AND VIV REDUCTION OF CYLINDRICAL STRUCTURES the specification of which is attached hereto unless the following box is checked:

☐ was filed on _____ as United States Application Number or PCT International Application Number _____ and was amended on _____ (if applicable).

I hereby state that I have reviewed and understand the contents of the above-identified specification, including the claims, as amended by any amendment referred to above.

I acknowledge the duty to disclose information which is material to patentability as defined in 37 CFR § 1.56.

I hereby claim foreign priority benefits under 35 U.S.C. § 119(a)-(d) or § 365(b) of any foreign application(s) for patent or inventor's certificate, or § 365(a) of any PCT International application which designated at least one country other than the United States, listed below and have also identified below by checking the box, any foreign application for patent or inventor's certificate, or PCT International application having a filing date before that of the application on which priority is claimed.

PRIOR FOREIGN APPLICATION(S)

Priority
Not Claimed

APPLICATION NUMBER	COUNTRY	DAY/MONTH/YEAR FILED	<input type="checkbox"/>
APPLICATION NUMBER	COUNTRY	DAY/MONTH/YEAR FILED	<input type="checkbox"/>

I hereby claim the benefit under 35 U.S.C. § 119(e) of any United States provisional application(s) listed below.

APPLICATION SERIAL NO.	FILING DATE
60/154,289	September 27, 1999
APPLICATION SERIAL NO.	FILING DATE

I hereby claim the benefit under 35 U.S.C. § 120 of any United States application(s) or § 365(c) of any PCT International application designating the United States, listed below and insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States or PCT International application in the manner provided by the first paragraph of 35 U.S.C. § 112, I acknowledge the duty to disclose information which is material to patentability as defined in 37 CFR § 1.56 which became available between the filing date of the prior application and the national or PCT International filing date of this application.

APPLICATION SERIAL NO.	FILING DATE	STATUS-PATENTED, PENDING, ABANDONED
APPLICATION SERIAL NO.	FILING DATE	STATUS-PATENTED, PENDING, ABANDONED

I hereby appoint the following attorney(s) and/or agent(s) to prosecute this application and to transact all business in the Patent and Trademark Office connected therewith:

NAME	ATTORNEY/AGENT	REGISTRATION NUMBER	TELEPHONE NUMBER
Mark A. Smith	Attorney	30,220	(713) 241-2094
NAME	ATTORNEY/AGENT	REGISTRATION NUMBER	TELEPHONE NUMBER
Dean F. Vance	Attorney	27,603	(713) 241-3716

Revised June 1995

SEND CORRESPONDENCE TO:

(NAME) **Mark A. Smith**
c/o Shell Oil Company
Intellectual Property
P.O. Box 2463
Houston, TX 77252-2463

DECLARATION AND POWER OF ATTORNEY FOR PATENT APPLICATION

ATTORNEY'S DOCKET NO.
TH-1258 (US)
MAS:KNL

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

FULL NAME OF SOLE OR FIRST INVENTOR (given name, family name)

Donald Wayne **ALLEN**

INVENTOR'S SIGNATURE

Donald Wayne Allen

DATE SIGNED

7/13/00

RESIDENCE

1806 Hillgreen Drive, Houston, Texas 77494

CITIZENSHIP

U.S.

POST OFFICE ADDRESS

1806 Hillgreen Drive, Houston, Texas 77494

FULL NAME OF SECOND JOINT INVENTOR, IF ANY (given name, family name)

Dean Leroy **HENNING**

SECOND INVENTOR'S SIGNATURE

Dean Leroy Henning

DATE SIGNED

07/13/00

RESIDENCE

3205 Hartledge Road, Needville, Texas 77461

CITIZENSHIP

U.S.

POST OFFICE ADDRESS

3205 Hartledge Road, Needville, Texas 77461

FULL NAME OF THIRD JOINT INVENTOR, IF ANY (given name, family name)

David Wayne **McMILLAN**

THIRD INVENTOR'S SIGNATURE

David Wayne McMillan

DATE SIGNED

7/13/00

RESIDENCE

1502 Tulsa Street, Deer Park, Texas 77536

CITIZENSHIP

U.S.

POST OFFICE ADDRESS

1502 Tulsa Street, Deer Park, Texas 77536

FULL NAME OF FOURTH JOINT INVENTOR, IF ANY (given name, family name)

Richard Bruce **McDANIEL**

FOURTH INVENTOR'S SIGNATURE

Richard Bruce McDaniel

DATE SIGNED

13/2/00

RESIDENCE

2919 Blue Wind Court, Houston, Texas 77084

CITIZENSHIP

U.S.

POST OFFICE ADDRESS

2919 Blue Wind Court, Houston, Texas 77084

FULL NAME OF FIFTH JOINT INVENTOR, IF ANY (given name, family name)

Kenneth **DUPAL**

FIFTH INVENTOR'S SIGNATURE

Kenneth Dupal

DATE SIGNED

18-114-00

RESIDENCE

9 Cristal Court, Mandeville, Louisiana 70448

CITIZENSHIP

U.S.

POST OFFICE ADDRESS

9 Cristal Court, Mandeville, Louisiana 70448